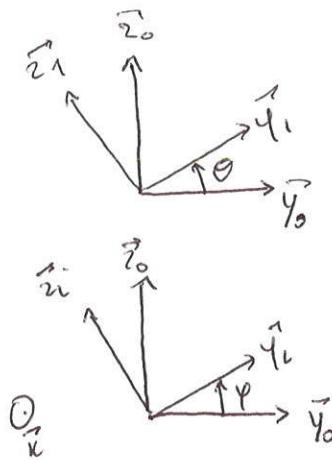
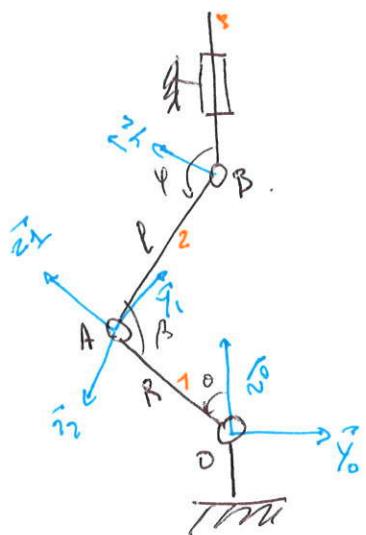


Objectif

Déterminer les efforts dans la liaison bielle manivelle sans prendre en compte de la combustion.

Schéma cinématique et repèresDétermination du champ de vitesse de la bielle

$$\vec{v}(2/0) = \vec{v}(2/1) + \vec{v}(1/0)$$

$$\vec{v}(1/0) = \dot{\theta} \vec{x}$$

$$\beta = 180 - \theta - (180 - \varphi).$$

$$\beta = \pi - \theta - \pi + \varphi$$

$$\vec{v}(2/0) = (\dot{\varphi} - \dot{\theta}) \vec{x}$$

$$= -\dot{\theta} + \dot{\varphi}.$$

$$\vec{v}(2/0) = \dot{\varphi} \vec{x} \quad (\text{car l'on ait au plus simplement en passant par } (3))$$

$$\text{Or } R \sin \theta = l \sin(\pi - \varphi) = l \sin \varphi. \quad \text{et} \quad \varphi = \pi - \text{Arcsin}\left(\frac{R \sin \theta}{l}\right).$$

$$\text{Ainsi } R \dot{\theta} \cos \theta = l \dot{\varphi} \cos \varphi.$$

$$\cos \varphi = -\frac{l}{R} \sqrt{l^2 - R^2 \sin^2 \theta}$$

$$R \dot{\theta} \cos \theta = l \dot{\varphi} \times \left(-\frac{1}{\frac{l}{R}}\right) \sqrt{l^2 - R^2 \sin^2 \theta}$$

$$\dot{\varphi} = -\frac{R \dot{\theta} \cos \theta}{\sqrt{l^2 - R^2 \sin^2 \theta}}$$

et donc 
$$\boxed{\vec{v}(2/0) = -\frac{R \dot{\theta} \cos \theta}{\sqrt{l^2 - R^2 \sin^2 \theta}} \vec{x}}$$

Et  $\boxed{\vec{v}_A(2/0) = \vec{v}_A(1/0) = -R \dot{\theta} \vec{y}}$

## Détermination du torseur cinétique de B bille en A

(2)

$$\vec{\tau}_A(2/0) = \eta_B \vec{AG} \wedge \vec{r}_A(2/0) + \underline{\underline{I}_G} \cdot \underline{\underline{\lambda}}(2/0).$$

$$\text{Notons } \vec{BG} = L, \vec{z}_L.$$

$\eta_B$ : Masse bille.

$$\underline{\underline{I}_G} = \begin{pmatrix} I_{xx} & 0 & 0 \\ 0 & I_{yy} & 0 \\ 0 & 0 & I_{zz} \end{pmatrix} (\vec{x}_B, \vec{y}_B, \vec{z}_B)$$

$$\text{Ainsi: } \vec{\tau}_A(2/0) = \eta_B (L - l_1) (-\vec{z}_L) \wedge (-R\dot{\theta}) \vec{y}_1 + \begin{pmatrix} I_{xx} & 0 & 0 \\ 0 & I_{yy} & 0 \\ 0 & 0 & I_{zz} \end{pmatrix} \begin{pmatrix} \lambda(2/0) \\ 0 \\ 0 \end{pmatrix},$$

$$\begin{aligned} \vec{y}_1 &= \cos \theta \vec{y}_0 + \sin \theta \vec{z}_0 \\ &= \cos \theta (\cos \varphi \vec{x}_L - \sin \varphi \vec{z}_L) + \sin \theta (\cos \varphi \vec{z}_L + \sin \varphi \vec{y}_L). \end{aligned}$$

$$\vec{y}_1 = \begin{pmatrix} 0 \\ \cos \theta \cos \varphi + \sin \theta \sin \varphi \\ \sin \theta \cos \varphi - \cos \theta \sin \varphi \end{pmatrix}$$

$$\tau_A(2/0) = -\eta_B (L - l_1) R\dot{\theta} \begin{pmatrix} 0 \\ 0 \\ -1 \end{pmatrix} \wedge \begin{pmatrix} 0 \\ \cos \theta \cos \varphi + \sin \theta \sin \varphi \\ \sin \theta \cos \varphi - \cos \theta \sin \varphi \end{pmatrix} + I_{xx} \lambda(2/0) \vec{n}.$$

$$\boxed{\tau_A(2/0) = [-\eta_B (L - l_1) R\dot{\theta} (\cos \theta \cos \varphi + \sin \theta \sin \varphi) + I_{xx} \lambda(2/0)] \vec{n}}$$

$$\text{et } \cos \varphi = -\frac{1}{\rho} \sqrt{\rho^2 - R^2 \sin^2 \theta} \quad \sin \varphi = \frac{R}{\rho} \sin \theta$$

(Passer sous cette forme pour ne pas déorder).

## Détermination de $\vec{v}_G(2/0)$ .

$$\vec{v}_G(2/0) = \vec{\tau}_A(2/0) + \underline{\underline{\lambda}}(2/0) \wedge \vec{AG}$$

$$= -R\dot{\theta} \vec{y}_1 + \underline{\underline{\lambda}}(2/0) \wedge (L - l_1) (-\vec{z}_L).$$

$$= -R\dot{\theta} \vec{y}_1 + \underline{\underline{\lambda}}(2/0) (L - l_1) \wedge \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \wedge \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}.$$

$$= -R\dot{\theta} \vec{y}_1 + (L - l_1) \underline{\underline{\lambda}}(2/0) \vec{y}_2$$

$$= -R\dot{\theta} (\cos \theta \vec{x}_0 + \sin \theta \vec{z}_0) + (L - l_1) \underline{\underline{\lambda}}(2/0) (\cos \varphi \vec{x}_L + \sin \varphi \vec{z}_L).$$

$$\boxed{\vec{v}_G(2/0) = [(L - l_1) \underline{\underline{\lambda}}(2/0) \cancel{\cos \varphi - R\dot{\theta} \cos \theta} \vec{y}_0 + [(L - l_1) \underline{\underline{\lambda}}(2/0) \sin \varphi + R\dot{\theta} \sin \theta] \vec{z}_0]}$$

Détermination du moment dynamique de la bielle en A... n°

(3)

$$\begin{aligned}\vec{s}_A(2/0) &= \frac{d}{dr} (\vec{r}_A(2/0)) + I_B \vec{v}_A(2/0) \wedge \vec{v}_B(2/0) \\ &= \frac{d}{dr} \left[ -I_B(\ell-l_1) R\dot{\theta} (\cos\theta \cos\varphi + \sin\theta \sin\varphi) + I_{nn} \ddot{\theta}(2/0) \right] \vec{x} \\ &\quad + I_B (-R\ddot{\theta}) \begin{pmatrix} 0 \\ \cos\theta \\ \sin\theta \end{pmatrix} \wedge \begin{pmatrix} 0 \\ (\ell-l_1) R(2/0) \cos\varphi - R\dot{\theta} \cos\theta \\ (\ell-l_1) R(2/0) \sin\varphi - R\dot{\theta} \sin\theta \end{pmatrix}.\end{aligned}$$

$$\begin{aligned}\vec{s}_A(2/0) &= \frac{d}{dr} \left[ -I_B(\ell-l_1) R\dot{\theta} (\cos\theta \cos\varphi + \sin\theta \sin\varphi) + I_{nn} \ddot{\theta}(2/0) \right] \vec{x} \\ &\quad + M_B (-R\ddot{\theta}) \left[ \cos\theta [(\ell-l_1) R(2/0) \sin\varphi - R\dot{\theta} \sin\theta] \right] \vec{y} \\ &\quad - \sin\theta [(\ell-l_1) \cos\varphi - R\dot{\theta} \cos\theta] \vec{z}\end{aligned}$$

Il faut exprimer avec  $\theta = 0$ :

$$\begin{aligned}&\frac{d}{dr} \left[ -I_B(\ell-l_1) R\dot{\theta} (\cos\theta \cos\varphi + \sin\theta \sin\varphi) + I_{nn} \ddot{\theta}(2/0) \right]. \\ &= \frac{d}{dr} \left[ -I_B(\ell-l_1) R\dot{\theta} \left( \cos\theta \left( \frac{-1}{\ell} \right) \sqrt{\ell^2 - R^2 \sin^2\theta} + \frac{R}{\ell} \sin^2\theta \right) + I_{nn} \ddot{\theta}(2/0) \right] \\ &= \frac{d}{dr} \left[ -I_B \frac{\ell-l_1}{\ell} R\dot{\theta} \left( R \sin^2\theta - \cos\theta \sqrt{\ell^2 - R^2 \sin^2\theta} \right) + I_{nn} \ddot{\theta}(2/0) \right] \\ &= -I_B \frac{\ell-l_1}{\ell} R\dot{\theta} \left[ \frac{d}{dr} (\sin^2\theta) - \frac{d}{dr} \left( \cos\theta \sqrt{\ell^2 - R^2 \sin^2\theta} \right) \right] + I_{nn} \frac{d}{dr} (\ddot{\theta}(2/0)) \\ &= -I_B \frac{\ell-l_1}{\ell} R\dot{\theta} \left[ R\dot{\theta} \sin 2\theta + \left( \sin\theta \sqrt{\ell^2 - R^2 \sin^2\theta} + \frac{R^2 \cos\theta \sin^2\theta}{\sqrt{\ell^2 - R^2 \sin^2\theta}} \right) \dot{\theta} \right] \\ &\quad + I_{nn} \frac{d}{dr} (\ddot{\theta}(2/0)) \\ \frac{d}{dr} (\vec{s}_A(2/0)) &= -I_B \frac{\ell-l_1}{\ell} R\dot{\theta}^2 \left[ R \sin 2\theta + \sin\theta \left[ \frac{\sqrt{\ell^2 - R^2 \sin^2\theta}}{2\sqrt{\ell^2 - R^2 \sin^2\theta}} + \frac{R^2 \sin 2\theta}{2(\ell^2 - R^2 \sin^2\theta)} \right] \right] + I_{nn} \frac{d}{dr} (\ddot{\theta}(2/0))\end{aligned}$$

~~réduire~~

$$\text{et } \frac{d}{dr} (\ddot{\theta}(2/0)) = -R\dot{\theta}^2 \left[ \frac{-\sin\theta}{\sqrt{\ell^2 - R^2 \sin^2\theta}} + \frac{R^2 \sin\theta \cos^2\theta}{(\ell^2 - R^2 \sin^2\theta)^{3/2}} \right]$$

$$\frac{d}{dr} (\ddot{\theta}(2/0)) = R\dot{\theta}^2 \left[ \frac{\sin\theta}{\sqrt{\ell^2 - R^2 \sin^2\theta}} - \frac{R^2 \sin\theta \cos^2\theta}{(\ell^2 - R^2 \sin^2\theta)^{3/2}} \right]$$

Determinanten der Acceleration des Kreisels

(4)

$$\vec{r}_6(2/0) = \begin{pmatrix} 0 \\ (L-L_1)\lambda(2/0) \cos\varphi - R\dot{\theta} \cos\Theta \\ (L-L_1)\lambda(2/0) \sin\varphi - R\dot{\theta} \sin\Theta \end{pmatrix}$$

$$\vec{s}_6(2/0) = \frac{d}{dr} [\vec{r}_6(2/0)]$$

$$= \begin{pmatrix} 0 \\ (L-L_1) \left[ \frac{d\lambda(2/0)}{dr} \cos\varphi + \lambda(2/0) \frac{d}{dr}(\cos\varphi) \right] + R\dot{\theta}^2 \sin\Theta \\ (L-L_1) \left[ \frac{d\lambda(2/0)}{dr} \sin\varphi + \lambda(2/0) \frac{d}{dr}(\sin\varphi) \right] - R\dot{\theta}^2 \cos\Theta \end{pmatrix}$$

$$\boxed{\vec{s}_6(2/0) = \begin{pmatrix} 0 \\ (L-L_1) \left( \frac{d\lambda(2/0)}{dr} \cos\varphi + (\lambda(2/0))^2 \sin\varphi \right) + R\dot{\theta}^2 \sin\Theta \\ (L-L_1) \left( \frac{d\lambda(2/0)}{dr} \sin\varphi + (\lambda(2/0))^2 \cos\varphi \right) - R\dot{\theta}^2 \cos\Theta \end{pmatrix}, (\vec{u}, \vec{q}_0, \vec{r}_0).}$$

Simplifiziere die Expression der  $\frac{d}{dr}(\vec{r}_A(2/0))$ .

$$\vec{r} \cdot \vec{J}_A(2/0) = -I_B(\bar{l}-l_1) R\dot{\theta} (\cos\Theta \cos\varphi + \sin\Theta \sin\varphi) + I_{nn} \lambda(2/0)$$

$$\frac{d \vec{r} \cdot \vec{J}_A(2/0)}{dr} = -I_B(\bar{l}-l_1) R\dot{\theta} \left[ \frac{d \cos\Theta \cos\varphi}{dr} + \cancel{\frac{d \sin\Theta \sin\varphi}{dr}} \right] + I_{nn} \frac{d \lambda(2/0)}{dr}$$

$$= -I_B(\bar{l}-l_1) R\dot{\theta} \left[ \dot{\theta} \sin\Theta \cos\varphi - \cancel{\lambda(2/0) \cos\Theta \sin\varphi} \right. \\ \left. + \dot{\theta} \cos\Theta \sin\varphi + \cancel{\lambda(2/0) \sin\Theta \cos\varphi} \right] + I_{nn} \frac{d \lambda(2/0)}{dr}$$

$$\boxed{\frac{d \vec{r} \cdot \vec{J}_A(2/0)}{dr} = -I_B(\bar{l}-l_1) R\dot{\theta} \left[ \dot{\theta} (\cos\Theta \sin\varphi - \sin\Theta \cos\varphi) + \lambda(2/0) (\sin\Theta \cos\varphi - \cos\Theta \sin\varphi) \right] + I_{nn} \frac{d \lambda(2/0)}{dr}}$$

Appliquer le PFS à la bielle

(5)

$$T_A(1 \rightarrow 2) = \begin{pmatrix} 0 & 0 \\ Y_{12} & 0 \\ Z_{12} & 0 \end{pmatrix}_{(\vec{x}, \vec{y}_0, \vec{z}_0)}$$

$$T_B(3 \rightarrow 2) = \begin{pmatrix} 0 & 0 \\ Y_{32} & 0 \\ Z_{32} & 0 \end{pmatrix}_{(\vec{x}, \vec{y}_0, \vec{z}_0)}$$

$$\vec{n}_A(3 \rightarrow 2) = \vec{n}_B(3 \rightarrow 2) + \vec{R}_B(3 \rightarrow 2) \wedge \vec{BA}$$

$$= \begin{pmatrix} 0 \\ Y_{32} \\ Z_{32} \end{pmatrix}_{(\vec{x}, \vec{y}_0, \vec{z}_0)} \wedge L \begin{pmatrix} 0 \\ -\sin \varphi \\ \cos \varphi \end{pmatrix} = L \begin{pmatrix} Y_{32} \cos \varphi + Z_{32} \sin \varphi \\ 0 \\ 0 \end{pmatrix}$$

$$\vec{n}_B(2/0) = R_A(1 \rightarrow 2) + R(3 \rightarrow 2)$$

Donc

$$\boxed{\begin{aligned} Y_{12} &= l_B(L-l_1) \left[ \frac{d \alpha(2/0)}{dr} \cos \varphi - (\alpha(2/0))^2 \sin \varphi \right] + R \dot{\theta}^L \sin \theta - Y_{32} \\ Z_{12} &= l_B(L-l_1) \left[ \frac{d \alpha(2/0)}{dr} \sin \varphi + (\alpha(2/0))^2 \cos \varphi \right] - R \dot{\theta}^L \cos \theta - Z_{32}. \end{aligned}}$$

Exprimer

$$\vec{v}_B(2/0) = \vec{v}_B(3/0)$$

~~Utilisation~~

$$\begin{aligned} \vec{v}_B(2/0) &= \vec{v}_A(2/0) + \vec{\omega}(2/0) \wedge \vec{AB} \\ &= -R \dot{\theta} \vec{q}_1 + -\frac{R \dot{\theta} \cos \theta}{\sqrt{P^2 - R^2 \sin^2 \theta}} \vec{n} \wedge (-l) \vec{z} \\ &= -R \dot{\theta} \vec{q}_1 + \frac{R \dot{\theta} \cos \theta}{\sqrt{P^2 - R^2 \sin^2 \theta}} \times L (-\vec{q}_2). \end{aligned}$$

Dans (o).

$$\begin{aligned} \vec{v}_B(2/0) &= -R \dot{\theta} (\cos \theta \vec{q}_0 + \sin \theta \vec{z}_0) + \frac{R \dot{\theta} \cos \theta \times L}{\sqrt{P^2 - R^2 \sin^2 \theta}} (\cos \varphi \vec{q}_0 + \sin \varphi \vec{z}_0) \\ &= -R \dot{\theta} (\cos \theta \vec{q}_0 + \sin \theta \vec{z}_0) + R \dot{\theta} \cos \theta \vec{q}_0 + -\frac{R \dot{\theta} \cos \theta \sin \theta}{\sqrt{P^2 - R^2 \sin^2 \theta}} \end{aligned}$$

$$\boxed{\vec{v}_B(2/0) = \left[ -R \dot{\theta} \sin \theta - \frac{R^2 \dot{\theta} \sin 2\theta}{2 \sqrt{P^2 - R^2 \sin^2 \theta}} \right] \vec{z}_0}$$

Appliquons le PFS au piston

$$m_p \frac{d\vec{v}_B(3/0)}{dr} = m_p \frac{d\vec{v}_B(2/0)}{dr} = \vec{R}(2 \rightarrow 3) + \vec{R}(0 \rightarrow 3)$$

$$m_p \frac{d\vec{v}_B(2/0)}{dr} \cdot \vec{e}_0 = Z_{23} + \overset{\text{2s2}}{\underset{0}{\text{Z}}} \quad (\text{Plan de glissement})$$

$$\Rightarrow Z_{23} = \overset{\text{1p}}{\underset{0}{\text{I}}} \frac{d}{dr} \left[ + R \dot{\theta} \sin \theta + \frac{R^2 \dot{\theta}^2 \sin 2\theta}{2\sqrt{P^2 - R^2 \sin^2 \theta}} \right].$$

~~$$Z_{23} = \overset{\text{1p}}{\underset{0}{\text{I}}} \frac{d}{dr} \left[ + R \dot{\theta} \cos \theta + \frac{R^2 \dot{\theta}^2 \cos 2\theta}{2\sqrt{P^2 - R^2 \sin^2 \theta}} \right]$$~~

$$Z_{23} = \left( + R \dot{\theta}^2 \cos \theta + \frac{R^2 \dot{\theta}^2 \cos 2\theta}{\sqrt{P^2 - R^2 \sin^2 \theta}} + \frac{R^4 \dot{\theta}^4 \sin^2 2\theta}{4(P^2 - R^2 \sin^2 \theta)^{3/2}} \right) \times \overset{\text{1p}}{\underset{0}{\text{I}}}.$$

Nombré dynamique en A

$$S_A(2/0) = L(\gamma_{32} \cos \varphi + Z_{23} \sin \varphi)$$

$$\Rightarrow \gamma_{32} = \frac{1}{\cos \varphi} \left[ \frac{S_A(2/0)}{L} - Z_{23} \sin \varphi \right].$$

Il suffit alors de reinjecter.